



## **Failure Modes, Effects and Diagnostic Analysis**

Project:

9116 Universal converter

Customer:

PR electronics A/S

Rønde

Denmark

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## Management summary

This report summarizes the results of the hardware assessment carried out on the 9116 Universal converter. The 9116 Universal converter consists of the versions 9116B1 / 9116B2 (Ex) and 9116A1 / 9116A2 (Standard). Table 1 gives an overview of the considered product variants.

A Failure Modes, Effects, and Diagnostic Analysis is one of the steps taken to achieve functional safety assessment of a device per IEC 61508 or ISO 13849. From the FMEDA, failure rates are determined and consequently the safety metrics for the corresponding standard can be calculated for a subsystem.

The FMEDA that is described in this report concerns only the hardware of the 9116 Universal converter. For full assessment purposes all requirements of IEC 61508 or ISO 13849 must be considered.

**Table 1: Overview of the considered Product variants**

	FMEDA name	HW/SW version	Configuration description
[C1]	3w Pt100 Aout	9116-1-V3R0	Resistance / RTD temperature / TC temperature inputs, Current Output
[C2]	3w Pt100 Relay	9116-1-V3R0	Resistance / RTD temperature / TC temperature inputs, Relay Output
[C3]	Current Aout	9116-1-V2R0	Current Input, Current Output
[C4]	Current Relay	9116-1-V2R0	Current input, Relay output
[C5]	Voltage Aout	9116-1-V2R0	Voltage input, Current Output
[C6]	Voltage Relay	9116-1-V2R0	Voltage input, Relay output

For safety applications only the described variants with the described hardware and software versions of the 9116 Universal converter have been considered. Any other variants and configurations are not covered by this report.

The 9116 Universal converter can be considered as a Type B <sup>1</sup> element with a hardware fault tolerance (HFT) of 0.

The failure modes and failure rates used in this analysis are from the *exida* Electrical Component Reliability Handbook [N2] for Profile 1. They meet the *exida* criteria for Route 2<sub>H</sub> (see Appendix 4). Therefore, the 9116 Universal converter can be classified as a 2<sub>H</sub> device when the listed failure rates are used. The analysis resulted in a DC (Diagnostic Coverage) of over 60%.

The failure rates are valid for the useful life of the 9116 Universal converter (see Appendix 2) when operating as defined in the considered scenarios.

When 2<sub>H</sub> data is used for all of the devices in an element, then the element meets the hardware architectural constraints up to SIL 2 at HFT=0 for low demand mode applications or SIL 2 / SIL 3 at HFT=1 for high and low demand mode applications.

It is assumed that the connected safety logic solver is configured as per the NAMUR NE43 signal ranges, i.e. the 9116 Universal converter with 4..20 mA current output communicates detected faults by an alarm output current  $\leq 3,6\text{mA}$  or  $\geq 21\text{mA}$ .

<sup>1</sup> Type B element: "Complex" element (using micro controllers or programmable logic); for details see 7.4.4.1.3 of IEC 61508-2:2010.

Assuming that, the application program in the safety logic solver does not automatically trip on these failures, these failures have been classified as dangerous detected failures. The following table shows how the above stated requirements are fulfilled.

**Table 2: Summary for the [C1] variant– IEC 61508 failure rates**

	<i>exida</i> Profile 1 <sup>2</sup>
<b>Failure category</b>	<b>Failure rates (in FIT)</b>
<b>Safe Detected (<math>\lambda_{SD}</math>)</b>	<b>0</b>
<b>Safe Undetected (<math>\lambda_{SU}</math>)</b>	<b>0</b>
<b>Dangerous Detected (<math>\lambda_{DD}</math>)</b>	<b>341</b>
Fail detected (detected by internal diagnostics)	249
Fail Low (detected by safety logic solver)	88
Fail high (detected by safety logic solver)	4
<b>Dangerous Undetected (<math>\lambda_{DU}</math>)</b>	<b>50</b>
<b>Total failure rate (safety function)</b>	<b>391</b>
<b>DC <sup>3</sup></b>	<b>87%</b>

**Table 3: Safety metrics according to ISO 13849-1 for the [C1] variant**

<b>MTTF<sub>D</sub> (years)</b>	<b>292 (High)</b>
<b>DC<sub>avg</sub></b>	<b>87% (Low)</b>
<b>Average frequency of a dangerous failure per hour (PFH) <sup>4</sup></b>	<b>5.03E-08 1/h</b>
<b>Performance Level (PL) <sup>5</sup></b>	<b>d</b>

<sup>2</sup> For details see Appendix 3.

<sup>3</sup> According to the Route 2<sub>H</sub> approach from IEC 61508, the DC value together with the device type is sufficient to derive the SIL level of the device. See chapter 4.4 for more details.

<sup>4</sup> The PFH value is only valid if the demand rate for the Safety Function is at least 100 times lower than the worst-case internal fault detection time.

<sup>5</sup> The complete Safety Function according to ISO 13849-1 needs to be evaluated to determine the overall achieved Performance Level. The Performance Level listed here only considers the MTTF<sub>D</sub>, DC<sub>avg</sub> and PFH value of the device itself.

**Table 4: Summary for the [C2] variant– IEC 61508 failure rates**

	<i>exida</i> Profile 1 <sup>6</sup>
Failure category	Failure rates (in FIT)
Safe Detected ( $\lambda_{SD}$ )	0
Safe Undetected ( $\lambda_{SU}$ )	77
Dangerous Detected ( $\lambda_{DD}$ )	235
Fail detected (detected by internal diagnostics)	235
Fail Low (detected by safety logic solver)	0
Fail high (detected by safety logic solver)	0
Dangerous Undetected ( $\lambda_{DU}$ )	70
<b>Total failure rate (safety function)</b>	<b>382</b>
<b>DC <sup>7</sup></b>	<b>77%</b>

**Table 5: Safety metrics according to ISO 13849-1 for the [C2] variant**

<b>MTTF<sub>D</sub> (years)</b>	<b>374 (High)</b>
<b>DC<sub>avg</sub></b>	<b>77% (Low)</b>
<b>Average frequency of a dangerous failure per hour (PFH) <sup>8</sup></b>	<b>7.00E-08 1/h</b>
<b>Performance Level (PL) <sup>9</sup></b>	<b>d</b>

<sup>6</sup> For details see Appendix 3.

<sup>7</sup> According to the Route 2<sub>H</sub> approach from IEC 61508, the DC value together with the device type is sufficient to derive the SIL level of the device. See chapter 4.4 for more details.

<sup>8</sup> The PFH value is only valid if the demand rate for the Safety Function is at least 100 times lower than the worst-case internal fault detection time.

<sup>9</sup> The complete Safety Function according to ISO 13849-1 needs to be evaluated to determine the overall achieved Performance Level. The Performance Level listed here only considers the MTTF<sub>D</sub>, DC<sub>avg</sub> and PFH value of the device itself.

**Table 6: Summary for the [C3] variant– IEC 61508 failure rates**

	<i>exida</i> Profile 1 <sup>10</sup>
Failure category	Failure rates (in FIT)
Safe Detected ( $\lambda_{SD}$ )	0
Safe Undetected ( $\lambda_{SU}$ )	0
Dangerous Detected ( $\lambda_{DD}$ )	487
Fail detected (detected by internal diagnostics)	310
Fail Low (detected by safety logic solver)	173
Fail high (detected by safety logic solver)	4
Dangerous Undetected ( $\lambda_{DU}$ )	51
<b>Total failure rate (safety function)</b>	<b>538</b>
<b>DC <sup>11</sup></b>	<b>91%</b>

**Table 7: Safety metrics according to ISO 13849-1 for the [C3] variant**

<b>MTTF<sub>D</sub> (years)</b>	<b>212 (High)</b>
<b>DC<sub>avg</sub></b>	<b>91% (Medium)</b>
<b>Average frequency of a dangerous failure per hour (PFH) <sup>12</sup></b>	<b>5.07E-08 1/h</b>
<b>Performance Level (PL) <sup>13</sup></b>	<b>d</b>

<sup>10</sup> For details see Appendix 3.

<sup>11</sup> According to the Route 2<sub>H</sub> approach from IEC 61508, the DC value together with the device type is sufficient to derive the SIL level of the device. See chapter 4.4 for more details.

<sup>12</sup> The PFH value is only valid if the demand rate for the Safety Function is at least 100 times lower than the worst-case internal fault detection time.

<sup>13</sup> The complete Safety Function according to ISO 13849-1 needs to be evaluated to determine the overall achieved Performance Level. The Performance Level listed here only considers the MTTF<sub>D</sub>, DC<sub>avg</sub> and PFH value of the device itself.

**Table 8: Summary for the [C4] variant– IEC 61508 failure rates**

<i>exida</i> Profile 1 <sup>14</sup>	
Failure category	Failure rates (in FIT)
<b>Safe Detected (<math>\lambda_{SD}</math>)</b>	<b>1</b>
<b>Safe Undetected (<math>\lambda_{SU}</math>)</b>	<b>166</b>
<b>Dangerous Detected (<math>\lambda_{DD}</math>)</b>	<b>297</b>
Fail detected (detected by internal diagnostics)	297
Fail Low (detected by safety logic solver)	0
Fail high (detected by safety logic solver)	0
<b>Dangerous Undetected (<math>\lambda_{DU}</math>)</b>	<b>71</b>
<b>Total failure rate (safety function)</b>	<b>535</b>
<b>DC <sup>15</sup></b>	<b>81%</b>

**Table 9: Safety metrics according to ISO 13849-1 for the [C4] variant**

<b>MTTF<sub>D</sub> (years)</b>	<b>310 (High)</b>
<b>DC<sub>avg</sub></b>	<b>81% (Low)</b>
<b>Average frequency of a dangerous failure per hour (PFH) <sup>16</sup></b>	<b>7.14E-08 1/h</b>
<b>Performance Level (PL) <sup>17</sup></b>	<b>d</b>

<sup>14</sup> For details see Appendix 3.

<sup>15</sup> According to the Route 2<sub>H</sub> approach from IEC 61508, the DC value together with the device type is sufficient to derive the SIL level of the device. See chapter 4.4 for more details.

<sup>16</sup> The PFH value is only valid if the demand rate for the Safety Function is at least 100 times lower than the worst-case internal fault detection time.

<sup>17</sup> The complete Safety Function according to ISO 13849-1 needs to be evaluated to determine the overall achieved Performance Level. The Performance Level listed here only considers the MTTF<sub>D</sub>, DC<sub>avg</sub> and PFH value of the device itself.

**Table 10: Summary for the [C5] variant– IEC 61508 failure rates**

	<i>exida</i> Profile 1 <sup>18</sup>
Failure category	Failure rates (in FIT)
Safe Detected ( $\lambda_{SD}$ )	0
Safe Undetected ( $\lambda_{SU}$ )	0
Dangerous Detected ( $\lambda_{DD}$ )	440
Fail detected (detected by internal diagnostics)	340
Fail Low (detected by safety logic solver)	97
Fail high (detected by safety logic solver)	3
Dangerous Undetected ( $\lambda_{DU}$ )	64
<b>Total failure rate (safety function)</b>	<b>504</b>
<b>DC <sup>19</sup></b>	<b>87%</b>

**Table 11: Safety metrics according to ISO 13849-1 for the [C5] variant**

<b>MTTF<sub>D</sub> (years)</b>	<b>226 (High)</b>
<b>DC<sub>avg</sub></b>	<b>87% (Low)</b>
<b>Average frequency of a dangerous failure per hour (PFH) <sup>20</sup></b>	<b>6.41E-08 1/h</b>
<b>Performance Level (PL) <sup>21</sup></b>	<b>d</b>

<sup>18</sup> For details see Appendix 3.

<sup>19</sup> According to the Route 2<sub>H</sub> approach from IEC 61508, the DC value together with the device type is sufficient to derive the SIL level of the device. See chapter 4.4 for more details.

<sup>20</sup> The PFH value is only valid if the demand rate for the Safety Function is at least 100 times lower than the worst-case internal fault detection time.

<sup>21</sup> The complete Safety Function according to ISO 13849-1 needs to be evaluated to determine the overall achieved Performance Level. The Performance Level listed here only considers the MTTF<sub>D</sub>, DC<sub>avg</sub> and PFH value of the device itself.

**Table 12: Summary for the [C6] variant– IEC 61508 failure rates**

	<i>exida</i> Profile 1 <sup>22</sup>
Failure category	Failure rates (in FIT)
<b>Safe Detected (<math>\lambda_{SD}</math>)</b>	<b>0</b>
<b>Safe Undetected (<math>\lambda_{SU}</math>)</b>	<b>111</b>
<b>Dangerous Detected (<math>\lambda_{DD}</math>)</b>	<b>379</b>
Fail detected (detected by internal diagnostics)	379
Fail Low (detected by safety logic solver)	0
Fail high (detected by safety logic solver)	0
<b>Dangerous Undetected (<math>\lambda_{DU}</math>)</b>	<b>98</b>
<b>Total failure rate (safety function)</b>	<b>588</b>
<b>DC <sup>23</sup></b>	<b>79%</b>

**Table 13: Safety metrics according to ISO 13849-1 for the [C6][C1] variant**

<b>MTTF<sub>D</sub> (years)</b>	<b>239 (High)</b>
<b>DC<sub>avg</sub></b>	<b>79% (Low)</b>
<b>Average frequency of a dangerous failure per hour (PFH) <sup>24</sup></b>	<b>9.82E-08 1/h</b>
<b>Performance Level (PL) <sup>25</sup></b>	<b>d</b>

These failure rates are valid for the useful lifetime of the product (see Appendix 2).

<sup>22</sup> For details see Appendix 3.

<sup>23</sup> According to the Route 2<sub>H</sub> approach from IEC 61508, the DC value together with the device type is sufficient to derive the SIL level of the device. See chapter 4.4 for more details.

<sup>24</sup> The PFH value is only valid if the demand rate for the Safety Function is at least 100 times lower than the worst-case internal fault detection time.

<sup>25</sup> The complete Safety Function according to ISO 13849-1 needs to be evaluated to determine the overall achieved Performance Level. The Performance Level listed here only considers the MTTF<sub>D</sub>, DC<sub>avg</sub> and PFH value of the device itself.



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## 1 Purpose and Scope

This document shall describe the results of the hardware assessment carried out on the 9116 Universal converter with hardware version 9116SMD\_2055.

The FMEDA builds the basis for an evaluation whether a sensor / logic / final-element subsystem, including the product, meets the average Probability of Failure on Demand ( $PFD_{AVG}$ ) / Probability of dangerous Failure per hour (PFH) requirements and the architectural constraints / minimum hardware fault tolerance requirements per IEC 61508 or ISO 13849.

It **does not** consider any calculations necessary for proving intrinsic safety or an evaluation of the correct device behavior in general. This FMEDA **does not** replace a full assessment according to IEC 61508 or ISO 13849.

## 2 Project management

### 2.1 *exida*

*exida* is one of the world's leading accredited Certification Bodies and knowledge companies specializing in automation system safety, availability, and cybersecurity with over 500 person years of cumulative experience in functional safety, alarm management, and cybersecurity. Founded by several of the world's top reliability and safety experts from manufacturers, operators and assessment organizations, *exida* is a global corporation with offices around the world. *exida* offers training, coaching, project oriented consulting services, safety engineering tools, detailed product assurance and ANSI accredited functional safety and cybersecurity certification. *exida* maintains a comprehensive failure rate and failure mode database on electronic and mechanical equipment and a comprehensive database on solutions to meet safety standards such as IEC 61508 or ISO 13849.

### 2.2 Roles of the parties involved

PR electronics A/S	Manufacturer of the 9116 Universal converter. PR electronics A/S performed the original FMEDA of the devices under consideration.
<i>exida</i>	Reviewed the original FMEDA from PR electronics A/S and transferred it to the latest SILcal X format. <i>exida</i> also updated the related FMEDA report to the <i>exida</i> CRD Route 2 <sub>H</sub> compliant failure rate data.

PR electronics A/S contracted *exida* in September 2023 with the update of the hardware assessment of the above mentioned device.

### 2.3 Standards / Literature used

The services delivered by *exida* were performed based on the following standards / literature.

[N1]	IEC 61508-2:2010	Functional Safety of Electrical/Electronic/Programmable Electronic Safety-Related Systems
[N2]	ISO 13849-1:2023	Safety of machinery — Safety-related parts of control systems — Part 1: General principles for design
[N3]	Component Reliability Database Handbook, 5th Edition, 2021 Vol. 1 – Electrical Components	<i>exida</i> LLC, Component Reliability Database Handbook, 5th Edition, 2021 Vol. 1 – Electrical Components ISBN 978-1-934977-09-5

### 2.4 *exida* tools used

[T1]	SILcal V6	FMEDA Tool
[T2]	exSILentia V4.13.0	SIL Verification Tool

## 2.5 Reference documents

### 2.5.1 Documentation provided by the customer

[D1]	9116 CPU failure distribution estimation.xls of 17.11.2023	Failure distribution for used CPUs
[D2]	9116 Circuit Description V2R0.doc of 11.02.10	Circuit description
[D3]	9116-1-04A-PDF.pdf of 02.03.2020	Circuit schematics and layout diagrams
[D4]	9116V100_DK.pdf of 2007.05.09	Users' manual (in Danish)
[D5]	9116 Derating Analysis.xls of 17.11.2023	Derating analysis
[D6]	9116 FMEDA 3W Pt100 RelayV0R8.xls of 15.11.2023	FMEDA results file generated by customer for 3w Pt100 Aout
[D7]	9116 FMEDA 3w Pt100 Aout V0R10.xls of 15.11.2023	FMEDA results file generated by customer for 3w Pt100 Relay
[D8]	9116 FMEDA Current Aout V0R10.xls of 16.11.2023	FMEDA results file generated by customer for 3w Current Aout
[D9]	9116 FMEDA Current Relay V0R10.xls of 16.11.2023	FMEDA results file generated by customer for 3w Current Relay
[D10]	9116 FMEDA Voltage Aout V0R10.xls of 16.11.2023	FMEDA results file generated by customer for 3w Voltage Aout
[D11]	9116 FMEDA Voltage Relay V0R10.xls of 16.11.2023	FMEDA results file generated by customer for 3w Voltage Relay
[D12]	9116V001.pdf of 2010.03.17	Users' manual (multilingual), from PRelectronics website.
[D13]	9116 Hardware Fault Insertion Test Report V2R0.doc of 11.02.10	Hardware Fault Insertion Test Report
[D14]	9116 Safety Manual V0R9.pdf	Safety Manual
[D15]	New A variant to the 9000 series of transmitters with grey terminals.msg of 15.05.14	Description of changes between Ex and standard versions.

The list above only means that the referenced documents were provided as basis for the FMEDA, but it does not mean that *exida* checked the correctness and completeness of these documents.

## 2.5.2 Documentation generated by *exida*

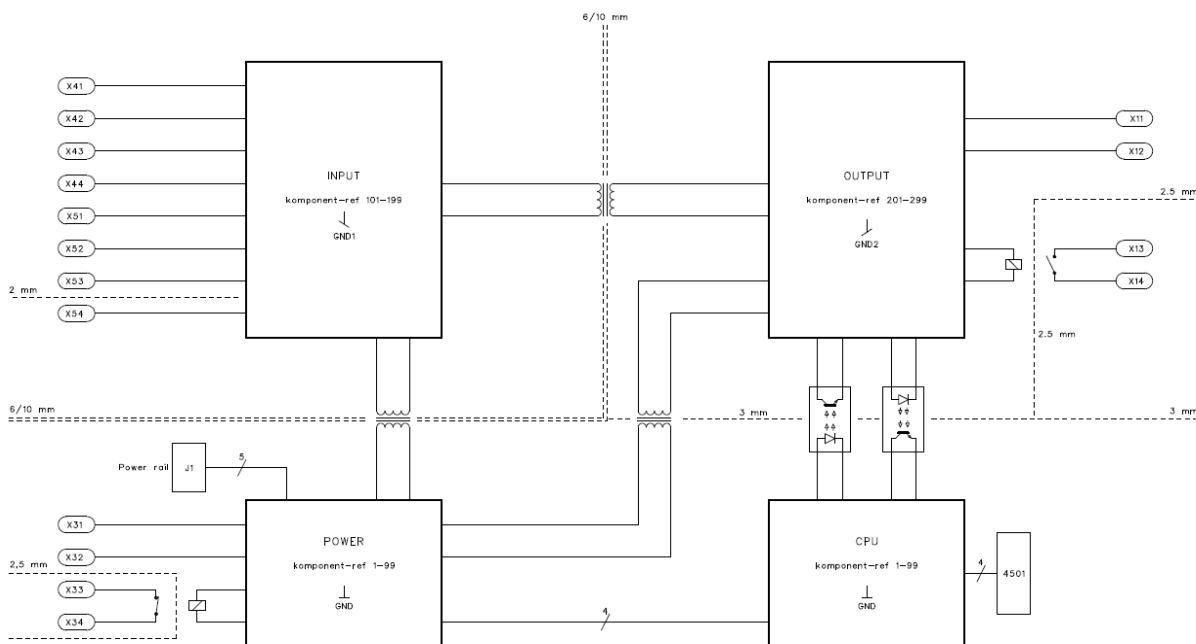
[R1]	9116 FMEDA 3w Pt100 Aout_CRD_5th_Ed_FIT_values.xlsx of 12.02.2024	FMEDA results file based on [D7] with Route 2 <sub>H</sub> compliant failure rate data used from the <i>exida</i> CRD [N3]
[R2]	9116 FMEDA 3W Pt100 Relay_CRD_5th_Ed_FIT_values.xlsx of 12.02.2024	FMEDA results file based on [D6] with Route 2 <sub>H</sub> compliant failure rate data used from the <i>exida</i> CRD [N3]
[R3]	9116 FMEDA Current Aout_CRD_5th_Ed_FIT_values.xlsx of 12.02.2024	FMEDA results file based on [D8] with Route 2 <sub>H</sub> compliant failure rate data used from the <i>exida</i> CRD [N3]
[R4]	9116 FMEDA Current Relay_CRD_5th_Ed_FIT_values.xlsx of 12.02.2024	FMEDA results file based on [D9] with Route 2 <sub>H</sub> compliant failure rate data used from the <i>exida</i> CRD [N3]
[R5]	9116 FMEDA Voltage Aout_CRD_5th_Ed_FIT_values.xlsx of 12.02.2024	FMEDA results file based on [D10] with Route 2 <sub>H</sub> compliant failure rate data used from the <i>exida</i> CRD [N3]
[R6]	9116 FMEDA Voltage Relay_CRD_5th_Ed_FIT_values.xlsx of 12.02.2024	FMEDA results file based on [D11] with Route 2 <sub>H</sub> compliant failure rate data used from the <i>exida</i> CRD [N3]

### 3 Product Description

The 9116 Universal converter converts various sensor input signals to either (1) a 4..20 mA current output, or to (2) a relay output.

The hardware for the 9116 Universal converter is divided into 4 major modules. Each of these modules is then divided in sub modules. In this document, all component functions of each sub module will be described. The general description of the modules is as follows:

- **MAIN SUPPLY:** Power supply circuit with external supply connection or from Power Rail. Additionally, this block contains the Status signal latching relay and the Power Rail status output.
- **MAIN CPU:** Contains the Main CPU circuit with front LEDS and interface to 4501 and Output.
- **INPUT:** Measurement circuits with ADC and a P to transfer measured values to Output. The input is isolated from the other modules with Ex-quality.
- **OUPUT:** Contains the Output P which handles all the main calculations, output current, output relay setting and the Ex isolation and power supply for Input.



**Figure 1: 9116 Universal converter circuit diagram**

As shown by Figure 2, the 9116 Universal converter has the following inputs: Input for RTD, TC, Ohm, potentiometer, mA and V. it has the following outputs: active mA output, passive mA output and relay output.

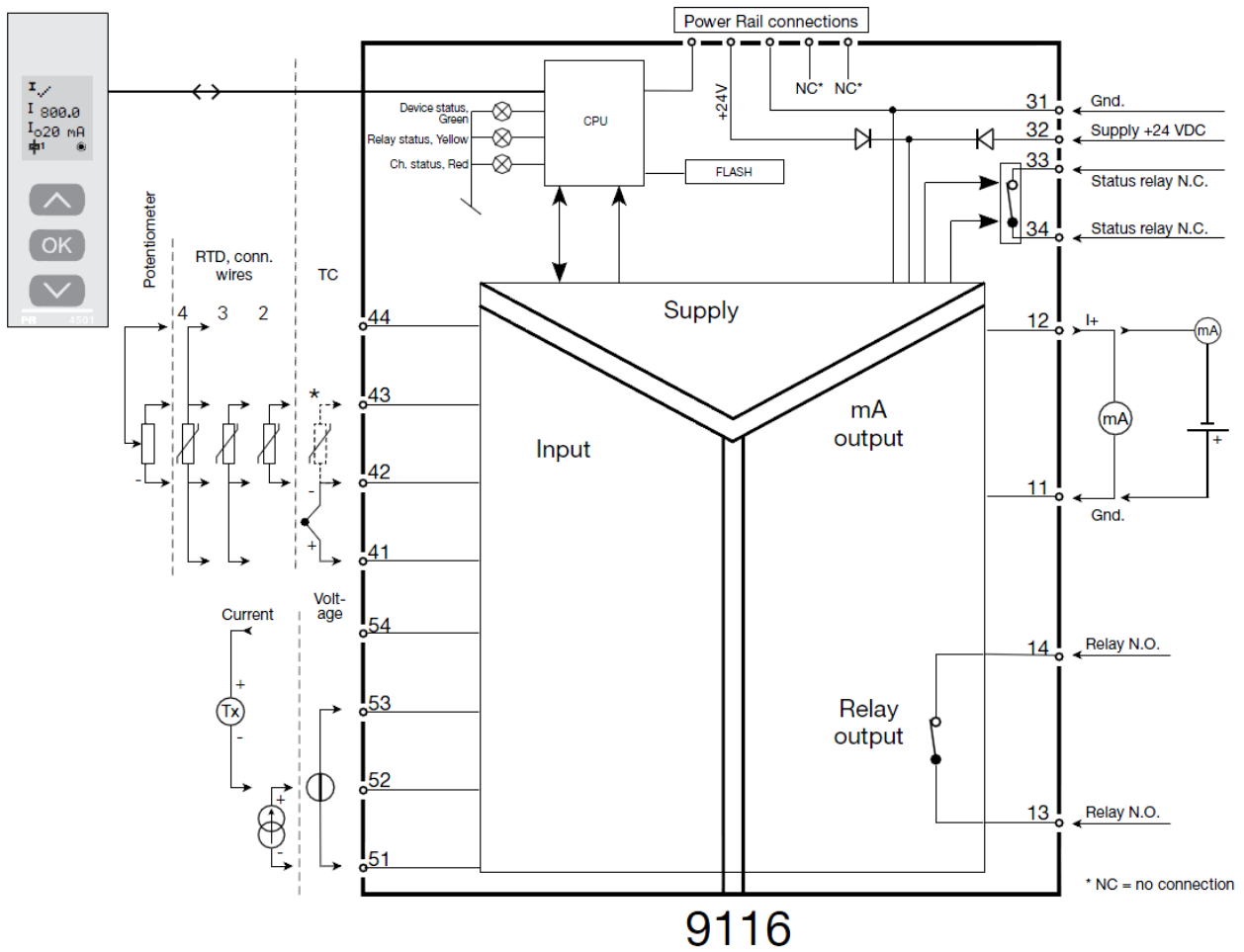


Figure 2: 9116 Universal converter block diagram

## 4 Failure Modes, Effects, and Diagnostic Analysis

The original Failure Modes, Effects, and Diagnostic Analysis was done by **PR electronics A/S** and is documented in [D6] to [D11]. *exida* updated the failure rates from that report to the *exida* CRD (see [N3]) and created the FMEDA documented in [R1] to [R6].

When the effect of a certain component failure mode could not be analyzed theoretically, the failure modes were introduced on component level and the effects of these failure modes were examined on system level (see fault insertion test report [D13]). This resulted in failures that can be classified according to the following failure categories.

### 4.1 Failure categories description

In order to judge the failure behavior of the 9116 Universal converter, the following definitions for the failure of the product were considered.

Fail-Safe State	For 3w Pt100 Aout, Current Aout, Voltage Aout, the fail-safe state is defined as the output reaching the user defined threshold value. For 3w Pt100 Relay, Current Relay, Voltage Relay, the fail-safe state is defined as the output being de-energized.
Fail Safe	Failure that causes the subsystem to go to the defined fail-safe state without a demand from the process.
Fail Dangerous	Failure that corrupts the measured value by more than 2% of full span (0.32mA) and therefore has the potential to not respond to a demand from the process (i.e. being unable to go to the defined fail-safe state).
Fail Dangerous Undetected	Failure that is dangerous and that is not being diagnosed by internal diagnostics.
Fail Dangerous Detected	Failure that is dangerous but is detected by internal diagnostics and causes the output signal to go to the predefined alarm state.
Fail High	A fail high failure (H) is defined as a failure that causes the output signal to go to the over-range or high alarm output current (> 21mA).
Fail Low	A fail low failure (L) is defined as a failure that causes the output signal to go to the under-range or low alarm output current (< 3.6mA).
No Effect	Failure mode of a component that plays a part in implementing the safety function but is neither a safe failure nor a dangerous failure and does not corrupt the measured value by more than 2% of full span (0.32mA).
Annunciation	Failure that does not directly impact safety but does impact the ability to detect a future fault (such as a fault in a diagnostic circuit).
No Part	Component that plays no part in implementing the safety function but is part of the circuit diagram and is listed for completeness. When calculating the DC, this failure mode is not taken into account. It is also not part of the total failure rate.

Depending on the application, a Fail High or a Fail Low failure can either be safe or dangerous and may be detected or undetected depending on the programming of the logic solver.





Consequently, during a Safety Integrity Level (SIL) verification assessment the Fail High and Fail Low failure categories need to be classified as safe or dangerous, detected or undetected.

The “Annunciation” failures are provided for those who wish to do reliability modeling more detailed than required by IEC 61508.

## 4.2 Methodology – FMEDA, Failure rates

### 4.2.1 FMEDA

A Failure Modes and Effects Analysis (FMEA) is a systematic way to identify and evaluate the effects of different component failure modes, to determine what could eliminate or reduce the chance of failure, and to document the system under consideration.

An FMEDA (Failure Mode Effect and Diagnostic Analysis) is an FMEA extension. It combines standard FMEA techniques with extensions to identify online diagnostics techniques and the failure modes relevant to safety instrumented system design. It is a technique recommended to generate failure rates for each important category (safe detected, safe undetected, dangerous detected, dangerous undetected, fail high, fail low) in the safety models. The format for the FMEDA is an extension of the standard FMEA format from MIL STD 1629A, Failure Modes and Effects Analysis.

### 4.2.2 Failure rates

The failure modes and failure rates used in this analysis are from the *exida* Electrical Component Reliability Handbook [N3] for environmental profile 1 (see Appendix 3). The rates were chosen in a way that is appropriate for safety integrity level verification calculations and the intended applications. It is expected that the actual number of field failures due to random events will be less than the number predicted by these failure rates.

For hardware assessment according to IEC 61508 or ISO 13849 only random equipment failures are of interest. It is assumed that the equipment has been properly selected for the application and is adequately commissioned such that early life failures (infant mortality) may be excluded from the analysis.

Early life failures (infant mortality) are not included in the failure rate prediction as it is assumed that some level of commission testing is done. End of life failures are not included in the failure rate prediction as useful life is specified.

Failures caused by external events should be considered as random failures. Examples of such failures are loss of power or physical abuse.

The assumption is also made that the equipment is maintained per the requirements of IEC 61508 or IEC 61511 and therefore a preventative maintenance program is in place to replace equipment before the end of its “useful life”.

The user of these numbers is responsible for determining the failure rate applicability to any particular environment.

Accurate plant specific data may be used to check validity of the failure rate data. If a user has data collected from a good proof test reporting system such as *exida* SILStat™ that indicates higher failure rates, the higher numbers shall be used.

### 4.2.3 Assumptions

The following assumptions have been made during the Failure Modes, Effects, and Diagnostic Analysis of the 9116 Universal converter.

- Failure rates are constant, wear out mechanisms are not included.
- Propagation of failures is not relevant.
- The device is installed per manufacturer's instructions.
- Failures during parameterization are not considered.
- Sufficient tests are performed prior to shipment to verify the absence of vendor and/or manufacturing defects that prevent proper operation of specified functionality to product specifications or cause operation different from the design analyzed.
- The Mean Time To Restoration (MTTR) after a safe failure is 24 hours.
- External power supply failure rates are not included.
- The time of a connected safety PLC to react on a dangerous detected failure and to bring the process to the safe state is identical to MTTR.
- Only the described versions are used for safety applications.
- Only one input and one output are part of the considered safety function.
- The application program in the safety logic solver is configured according to NAMUR NE43 to detect under-range and over-range failures and does not automatically trip on these failures; therefore these failures have been classified as dangerous detected failures.
- Materials are compatible with process conditions.
- The measurement / application limits (including pressure and temperature ranges) are considered.
- Short circuit and lead breakage detection are activated.
- The worst-case internal fault detection time is 30 seconds. Therefore, a demand for the safety function in high demand mode is only possible every 3000 seconds<sup>26</sup>, which corresponds to 50 minutes.
- Soft Error Rates (SER) were considered for relative neutron flux of 4.5 corresponding to 1,600 meters above sea.

### 4.3 FMEDA Results

For the calculations the following has to be noted:

$$\lambda_{\text{total}} = \lambda_{\text{SD}} + \lambda_{\text{SU}} + \lambda_{\text{DD}} + \lambda_{\text{DU}}$$

#### IEC 61508:

$$\text{DC} = \lambda_{\text{DD}} / (\lambda_{\text{DD}} + \lambda_{\text{DU}})$$

#### ISO 13849-1:

$$\text{MTTF}_D [\text{years}] = 1 / ((\lambda_{\text{DD}} + \lambda_{\text{DU}}) * 24 * 365)$$

$$\text{PFH} = \lambda_{\text{DU}}$$

$$\text{DC}_{\text{avg}} = \lambda_{\text{DD}} / (\lambda_{\text{DD}} + \lambda_{\text{DU}})$$

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<sup>26</sup> See IEC 61508-2:2010, paragraph 7.4.4.1.4 and ISO 13849-1:2023, paragraph 6.1.3.2.4

### 4.3.1 9116 Universal converter

The FMEDA carried out on the 9116 Universal converter in the product variants [C1] to [C6] under the assumptions described in section 4.2.3 and the definitions given in section 4.1 and 4.2 leads to the following failure rates:

**Table 14: Summary for the [C1] variant– IEC 61508 failure rates**

	<i>exida</i> Profile 1 <sup>27</sup>
<b>Failure category</b>	<b>Failure rates (in FIT)</b>
<b>Safe Detected (<math>\lambda_{SD}</math>)</b>	<b>0</b>
<b>Safe Undetected (<math>\lambda_{SU}</math>)</b>	<b>0</b>
<b>Dangerous Detected (<math>\lambda_{DD}</math>)</b>	<b>341</b>
Fail detected (detected by internal diagnostics)	249
Fail low (detected by safety logic solver)	88
Fail high (detected by safety logic solver)	4
<b>Dangerous Undetected (<math>\lambda_{DU}</math>)</b>	<b>50</b>
Annunciation ( $\lambda_A$ )	33
No effect ( $\lambda_{\#}$ )	191
No part ( $\lambda_{-}$ )	645
<b>Total failure rate (safety function)</b>	<b>391</b>
<b>DC <sup>28</sup></b>	<b>87%</b>

<sup>27</sup> For details see Appendix 3.

<sup>28</sup> According to the Route 2<sub>H</sub> approach from IEC 61508, the DC value together with the device type is sufficient to derive the SIL level of the device. See chapter 4.4 for more details.

Table 15: Safety metrics according to ISO 13849-1 for the [C1] variant

MTTF <sub>D</sub> (years)	292 (High)
DC <sub>avg</sub>	87% (Low)
Average frequency of a dangerous failure per hour (PFH) <sup>29</sup>	5.03E-08 1/h
Performance Level (PL) <sup>30</sup>	d

<sup>29</sup> The PFH value is only valid if the demand rate for the Safety Function is at least 100 times lower than the worst-case internal fault detection time.

<sup>30</sup> The complete Safety Function according to ISO 13849-1 needs to be evaluated to determine the overall achieved Performance Level. The Performance Level listed here only considers the MTTF<sub>D</sub>, DC<sub>avg</sub> and PFH value of the device itself.

**Table 16: Summary for the [C2] variant– IEC 61508 failure rates**

<i>exida</i> Profile 1 <sup>31</sup>	
<b>Failure category</b>	<b>Failure rates (in FIT)</b>
<b>Safe Detected (<math>\lambda_{SD}</math>)</b>	<b>0</b>
<b>Safe Undetected (<math>\lambda_{SU}</math>)</b>	<b>77</b>
<b>Dangerous Detected (<math>\lambda_{DD}</math>)</b>	<b>235</b>
Fail detected (detected by internal diagnostics)	235
Fail low (detected by safety logic solver)	0
Fail high (detected by safety logic solver)	0
<b>Dangerous Undetected (<math>\lambda_{DU}</math>)</b>	<b>70</b>
Annunciation ( $\lambda_A$ )	27
No effect ( $\lambda_{\#}$ )	178
No part ( $\lambda_{-}$ )	672
<b>Total failure rate (safety function)</b>	<b>382</b>
<b>DC <sup>32</sup></b>	<b>77%</b>

**Table 17: Safety metrics according to ISO 13849-1 for the [C2] variant**

<b>MTTF<sub>D</sub> (years)</b>	<b>374 (High)</b>
<b>DC<sub>avg</sub></b>	<b>77% (Low)</b>
<b>Average frequency of a dangerous failure per hour (PFH) <sup>33</sup></b>	<b>7.00E-08 1/h</b>
<b>Performance Level (PL) <sup>34</sup></b>	<b>d</b>

<sup>31</sup> For details see Appendix 3.

<sup>32</sup> According to the Route 2<sub>H</sub> approach from IEC 61508, the DC value together with the device type is sufficient to derive the SIL level of the device. See chapter 4.4 for more details.

<sup>33</sup> The PFH value is only valid if the demand rate for the Safety Function is at least 100 times lower than the worst-case internal fault detection time.

<sup>34</sup> The complete Safety Function according to ISO 13849-1 needs to be evaluated to determine the overall achieved Performance Level. The Performance Level listed here only considers the MTTF<sub>D</sub>, DC<sub>avg</sub> and PFH value of the device itself.

**Table 18: Summary for the [C3] variant– IEC 61508 failure rates**

<i>exida</i> Profile 1 <sup>35</sup>	
<b>Failure category</b>	<b>Failure rates (in FIT)</b>
<b>Safe Detected (<math>\lambda_{SD}</math>)</b>	<b>0</b>
<b>Safe Undetected (<math>\lambda_{SU}</math>)</b>	<b>0</b>
<b>Dangerous Detected (<math>\lambda_{DD}</math>)</b>	<b>487</b>
Fail detected (detected by internal diagnostics)	310
Fail low (detected by safety logic solver)	173
Fail high (detected by safety logic solver)	4
<b>Dangerous Undetected (<math>\lambda_{DU}</math>)</b>	<b>51</b>
Annunciation ( $\lambda_A$ )	33
No effect ( $\lambda_{\#}$ )	300
No part ( $\lambda_{-}$ )	389
<b>Total failure rate (safety function)</b>	<b>538</b>
<b>DC <sup>36</sup></b>	<b>91%</b>

**Table 19: Safety metrics according to ISO 13849-1 for the [C3] variant**

<b>MTTF<sub>D</sub> (years)</b>	<b>212 (High)</b>
<b>DC<sub>avg</sub></b>	<b>91% (Medium)</b>
<b>Average frequency of a dangerous failure per hour (PFH) <sup>37</sup></b>	<b>5.07E-08 1/h</b>
<b>Performance Level (PL) <sup>38</sup></b>	<b>d</b>

<sup>35</sup> For details see Appendix 3.

<sup>36</sup> According to the Route 2<sub>H</sub> approach from IEC 61508, the DC value together with the device type is sufficient to derive the SIL level of the device. See chapter 4.4 for more details.

<sup>37</sup> The PFH value is only valid if the demand rate for the Safety Function is at least 100 times lower than the worst-case internal fault detection time.

<sup>38</sup> The complete Safety Function according to ISO 13849-1 needs to be evaluated to determine the overall achieved Performance Level. The Performance Level listed here only considers the MTTF<sub>D</sub>, DC<sub>avg</sub> and PFH value of the device itself.

**Table 20: Summary for the [C4] variant– IEC 61508 failure rates**

<i>exida</i> Profile 1 <sup>39</sup>	
<b>Failure category</b>	<b>Failure rates (in FIT)</b>
<b>Safe Detected (<math>\lambda_{SD}</math>)</b>	<b>1</b>
<b>Safe Undetected (<math>\lambda_{SU}</math>)</b>	<b>166</b>
<b>Dangerous Detected (<math>\lambda_{DD}</math>)</b>	<b>297</b>
Fail detected (detected by internal diagnostics)	297
Fail low (detected by safety logic solver)	0
Fail high (detected by safety logic solver)	0
<b>Dangerous Undetected (<math>\lambda_{DU}</math>)</b>	<b>71</b>
Annunciation ( $\lambda_A$ )	27
No effect ( $\lambda_{\#}$ )	290
No part ( $\lambda_{-}$ )	426
<b>Total failure rate (safety function)</b>	<b>535</b>
<b>DC <sup>40</sup></b>	<b>81%</b>

**Table 21: Safety metrics according to ISO 13849-1 for the [C4] variant**

<b>MTTF<sub>D</sub> (years)</b>	<b>310 (High)</b>
<b>DC<sub>avg</sub></b>	<b>81% (Low)</b>
<b>Average frequency of a dangerous failure per hour (PFH) <sup>41</sup></b>	<b>7.14E-08 1/h</b>
<b>Performance Level (PL) <sup>42</sup></b>	<b>d</b>

<sup>39</sup> For details see Appendix 3.

<sup>40</sup> According to the Route 2<sub>H</sub> approach from IEC 61508, the DC value together with the device type is sufficient to derive the SIL level of the device. See chapter 4.4 for more details.

<sup>41</sup> The PFH value is only valid if the demand rate for the Safety Function is at least 100 times lower than the worst-case internal fault detection time.

<sup>42</sup> The complete Safety Function according to ISO 13849-1 needs to be evaluated to determine the overall achieved Performance Level. The Performance Level listed here only considers the MTTF<sub>D</sub>, DC<sub>avg</sub> and PFH value of the device itself.



**Table 22: Summary for the [C5] variant– IEC 61508 failure rates**

<i>exida</i> Profile 1 <sup>43</sup>	
Failure category	Failure rates (in FIT)
<b>Safe Detected (<math>\lambda_{SD}</math>)</b>	<b>0</b>
<b>Safe Undetected (<math>\lambda_{SU}</math>)</b>	<b>0</b>
<b>Dangerous Detected (<math>\lambda_{DD}</math>)</b>	<b>440</b>
Fail detected (detected by internal diagnostics)	340
Fail low (detected by safety logic solver)	97
Fail high (detected by safety logic solver)	3
<b>Dangerous Undetected (<math>\lambda_{DU}</math>)</b>	<b>64</b>
Annunciation ( $\lambda_A$ )	33
No effect ( $\lambda_{\#}$ )	269
No part ( $\lambda_{-}$ )	454
<b>Total failure rate (safety function)</b>	<b>504</b>
<b>DC <sup>44</sup></b>	<b>87%</b>

**Table 23: Safety metrics according to ISO 13849-1 for the [C5] variant**

<b>MTTF<sub>D</sub> (years)</b>	<b>226 (High)</b>
<b>DC<sub>avg</sub></b>	<b>87% (Low)</b>
<b>Average frequency of a dangerous failure per hour (PFH) <sup>45</sup></b>	<b>6.41E-08 1/h</b>
<b>Performance Level (PL) <sup>46</sup></b>	<b>d</b>

<sup>43</sup> For details see Appendix 3.

<sup>44</sup> According to the Route 2<sub>H</sub> approach from IEC 61508, the DC value together with the device type is sufficient to derive the SIL level of the device. See chapter 4.4 for more details.

<sup>45</sup> The PFH value is only valid if the demand rate for the Safety Function is at least 100 times lower than the worst-case internal fault detection time.

<sup>46</sup> The complete Safety Function according to ISO 13849-1 needs to be evaluated to determine the overall achieved Performance Level. The Performance Level listed here only considers the MTTF<sub>D</sub>, DC<sub>avg</sub> and PFH value of the device itself.

**Table 24: Summary for the [C6] variant– IEC 61508 failure rates**

<i>exida</i> Profile 1 <sup>47</sup>	
<b>Failure category</b>	<b>Failure rates (in FIT)</b>
<b>Safe Detected (<math>\lambda_{SD}</math>)</b>	<b>0</b>
<b>Safe Undetected (<math>\lambda_{SU}</math>)</b>	<b>111</b>
<b>Dangerous Detected (<math>\lambda_{DD}</math>)</b>	<b>379</b>
Fail detected (detected by internal diagnostics)	379
Fail low (detected by safety logic solver)	0
Fail high (detected by safety logic solver)	0
<b>Dangerous Undetected (<math>\lambda_{DU}</math>)</b>	<b>98</b>
Annunciation ( $\lambda_A$ )	22
No effect ( $\lambda_{\#}$ )	883
No part ( $\lambda_{-}$ )	47
<b>Total failure rate (safety function)</b>	<b>588</b>
<b>DC <sup>48</sup></b>	<b>79%</b>

**Table 25: Safety metrics according to ISO 13849-1 for the [C6] variant**

<b>MTTF<sub>D</sub> (years)</b>	<b>239 (High)</b>
<b>DC<sub>avg</sub></b>	<b>79% (Low)</b>
<b>Average frequency of a dangerous failure per hour (PFH) <sup>49</sup></b>	<b>9.82E-08 1/h</b>
<b>Performance Level (PL) <sup>50</sup></b>	<b>d</b>

These failure rates are valid for the useful lifetime of the product (see Appendix 2).

<sup>47</sup> For details see Appendix 3.

<sup>48</sup> According to the Route 2<sub>H</sub> approach from IEC 61508, the DC value together with the device type is sufficient to derive the SIL level of the device. See chapter 4.4 for more details.

<sup>49</sup> The PFH value is only valid if the demand rate for the Safety Function is at least 100 times lower than the worst-case internal fault detection time.

<sup>50</sup> The complete Safety Function according to ISO 13849-1 needs to be evaluated to determine the overall achieved Performance Level. The Performance Level listed here only considers the MTTF<sub>D</sub>, DC<sub>avg</sub> and PFH value of the device itself.

#### 4.4 Architectural Constraints

The architectural constraint type for the 9116 Universal converter is B. The hardware fault tolerance of the device is 0.

According to IEC 61508 the architectural constraints of an element must be determined. This can be done by following the 1<sub>H</sub> approach according to 7.4.4.2 of IEC 61508-2 or the 2<sub>H</sub> approach according to 7.4.4.3 of IEC 61508-2.

The 1<sub>H</sub> approach involves calculating the Safe Failure Fraction (SFF) for the entire element.

The 2<sub>H</sub> approach involves assessment of the reliability data for the entire element according to 7.4.4.3.3 of IEC 61508-2.

This FMEDA analysis uses the 2<sub>H</sub> approach with the 2<sub>H</sub> qualified failure rates from the *exida* component reliability database [N3] (see also Appendix 4). To apply the 2<sub>H</sub> approach on a Type B device, the diagnostic coverage has to be at least 60%.

The analysis shows that the lowest diagnostic coverage for the 9116 Universal converter device series is 77% (applies for the [C2] product variant) and therefore, the whole device series meets the hardware architectural constraints for up to SIL 2.

When 2<sub>H</sub> data is used for all of the devices in an element, then the element meets the hardware architectural constraints up to SIL 2 at HFT=0 for low demand mode applications or SIL 2 / SIL 3 at HFT=1 for high and low demand mode applications.

As the 9116 Universal converter is only one part of an element, the architectural constraints should be determined for the entire sensor element.

The SIS designer is responsible for meeting other requirements of applicable standards for any given SIL.

## 5 Using the FMEDA results

Using the failure rate data given in section 4.3.1 and the failure rate data for the associated element devices, an average Probability of Failure on Demand ( $PFD_{AVG}$ ) calculation can be performed for the entire Safety Instrumented Function (SIF).

Probability of Failure on Demand ( $PFD_{AVG}$ ) calculation uses several parameters, many of which are determined by the particular application and the operational policies of each site. Some parameters are product specific and the responsibility of the manufacturer. Those manufacturer specific parameters are given in this third party report.

To perform an average Probability of Failure on Demand ( $PFD_{AVG}$ ) calculation is the responsibility of the owner/operator of a process and is often delegated to the SIF designer. Product manufacturers can only provide a  $PFD_{AVG}$  by making many assumptions about the application and operational policies of a site. Therefore, use of these numbers requires complete knowledge of the assumptions and a match with the actual application and site.

Probability of Failure on Demand ( $PFD_{AVG}$ ) calculation is best accomplished with *exida's* exSILentia tool.

The failure rates for all the devices of the Safety Instrumented Function and the corresponding proof test coverages are required to perform the  $PFD_{AVG}$  calculation. The proof test coverage of the suggested proof test for the 9116 Universal converter is listed in Appendix 1.1. This has to be combined with the dangerous failure rates after proof test for other devices to establish the proof test coverage for the entire Safety Instrumented Function.

When performing testing at regular intervals, the 9116 Universal converter contribute less to the overall  $PFD_{AVG}$  of the safety instrumented function.

The following section gives a simplified example on how to apply the results of the FMEDA.

## 5.1 Example PFD<sub>AVG</sub> / PFH calculation

An average Probability of Failure on Demand (PFD<sub>AVG</sub>) calculation is performed for a single (1oo1) 9116 Universal converter with *exida's* exSILentia tool. The failure rate data used in this calculation are given in section 4.3.1.

A mission time of 10 years has been assumed, a Mean Time To Restoration of 24 hours and a maintenance capability of 100%. Table 26 lists the results for different proof test intervals considering an average proof test coverage of 95% (see Appendix 1.1).

**Table 26: 9116 Universal converter – PFD<sub>AVG</sub> / PFH values**

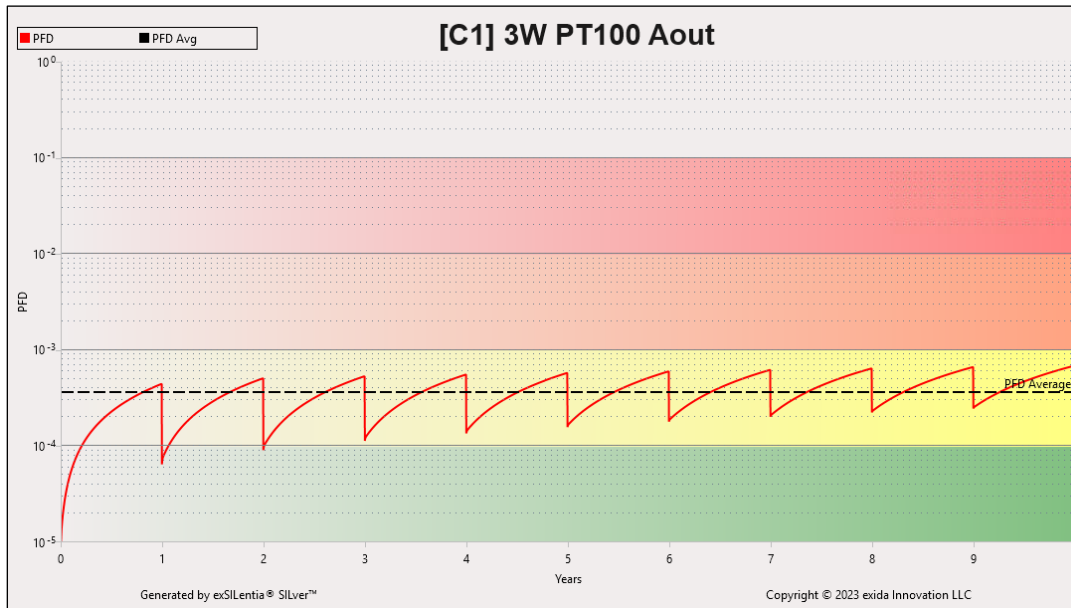
Configuration	PFH [1/h]	T[Proof] = 1 year	T[Proof] = 4 years
3w Pt100 Aout	PFH = 5.03E-08	PFD <sub>AVG</sub> = 3.70E-04	PFD <sub>AVG</sub> = 9.76E-04
3w Pt100 Relay	PFH = 7.00E-08	PFD <sub>AVG</sub> = 5.08E-04	PFD <sub>AVG</sub> = 1.35E-03
Current Aout	PFH = 5.07E-08	PFD <sub>AVG</sub> = 3.76E-04	PFD <sub>AVG</sub> = 9.87E-04
Current Relay	PFH = 7.14E-08	PFD <sub>AVG</sub> = 5.19E-04	PFD <sub>AVG</sub> = 1.38E-03
Voltage Aout	PFH = 6.41E-08	PFD <sub>AVG</sub> = 4.71E-04	PFD <sub>AVG</sub> = 9.54E-04
Voltage Relay	PFH = 9.82E-08	PFD <sub>AVG</sub> = 7.13E-04	PFD <sub>AVG</sub> = 1.90E-03

For SIL2 the overall PFD<sub>AVG</sub> shall be better than 1.00E-02 and the PFH shall be better than 1.00E-06 1/h.

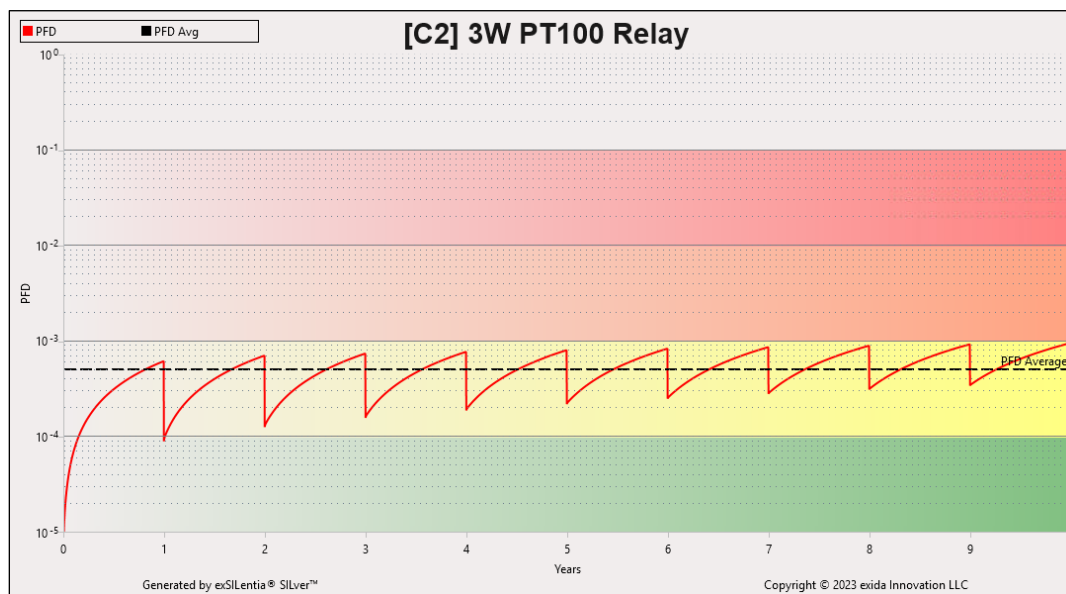
As the 9116 Universal converter is contributing to the entire safety function, it should only consume a certain percentage of the allowed range. Assuming 10% of this range as a reasonable budget, they should be better than or equal to a PFD<sub>AVG</sub> value of 1.00E-03 or a PFH value of 1.00E-07 1/h, respectively.

With a proof test interval of one year, the calculated PFD<sub>AVG</sub> / PFH values are within the allowed range for SIL 2 according to table 2 of IEC 61508-1:2010 and do fulfill the assumption to not claim more than 10% of the allowed range, i.e. to be better than or equal to 1.00E-03 or 1.00E-07 1/h, respectively.

The resulting PFD(t) / PFD<sub>AVG</sub> graph generated with exSILentia for a proof test interval of one year is displayed in Figure 3.



**Figure 3: PFD(t) / PFD<sub>AVG</sub> for [C1]**



**Figure 4: PFD(t) / PFD<sub>AVG</sub> for [C2]**

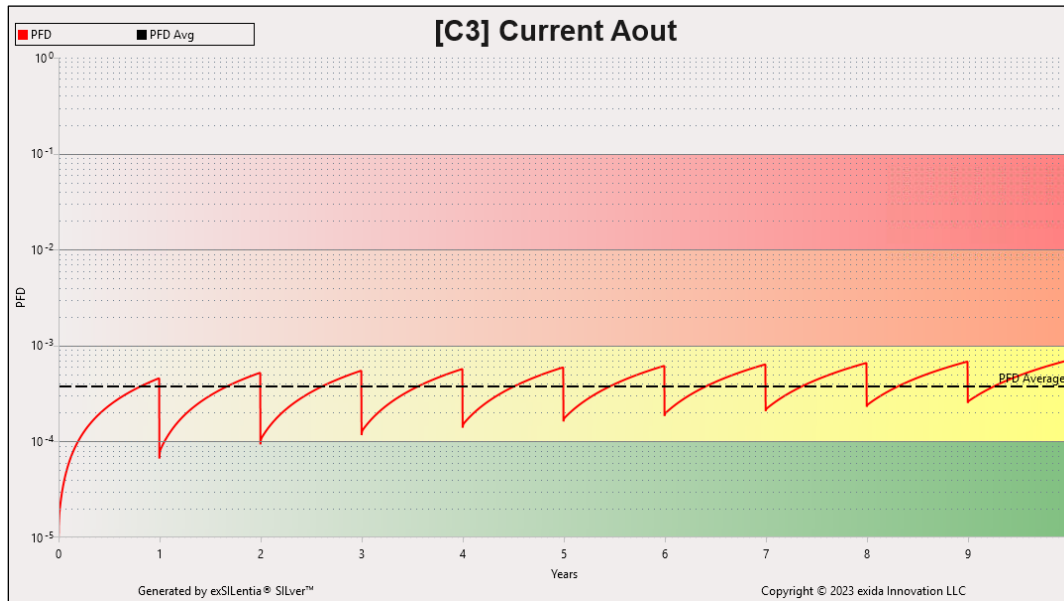


Figure 5: PFD(t) / PFDAVG for [C3]

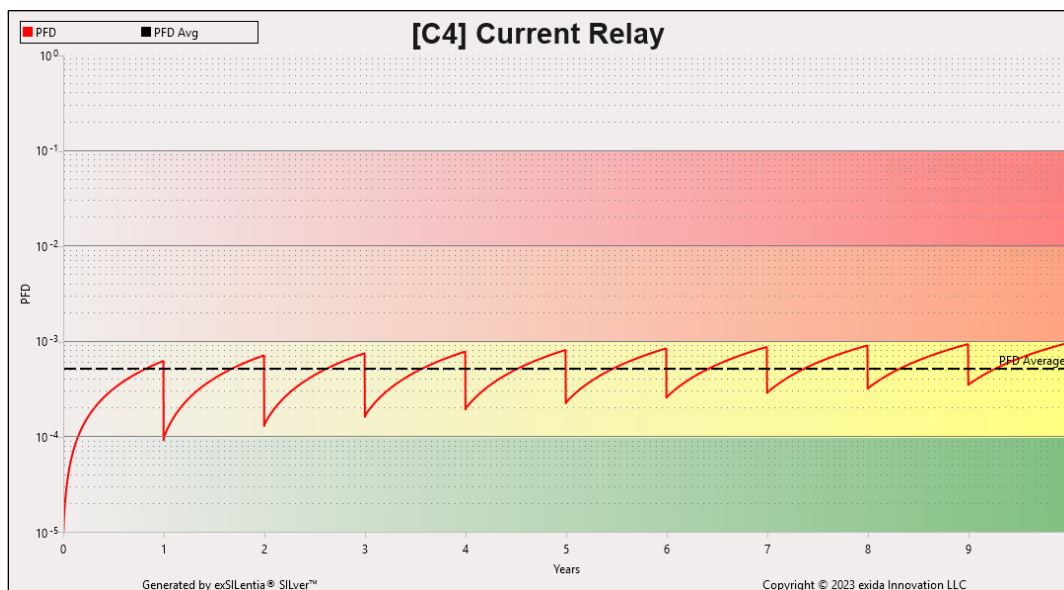
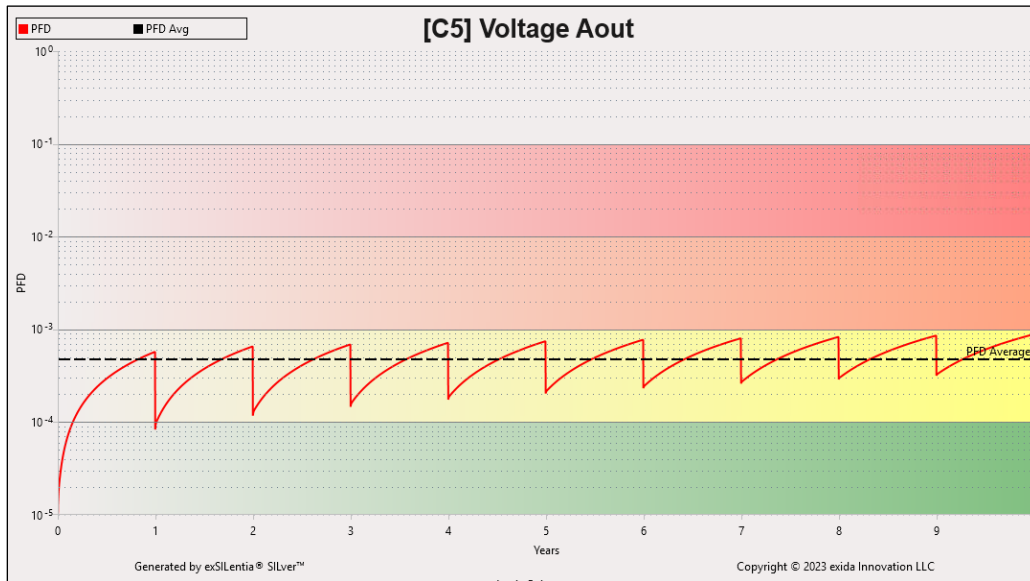
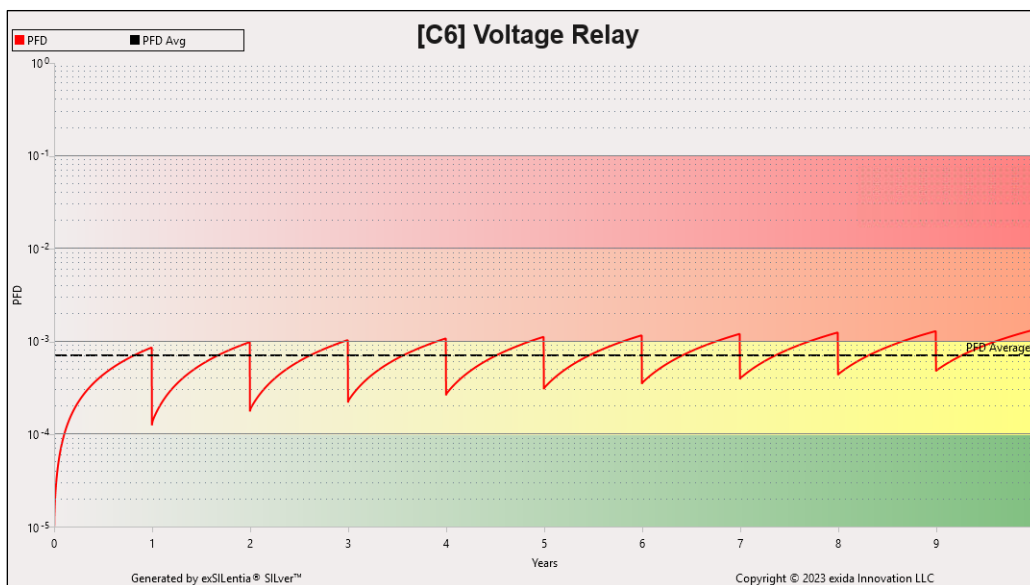


Figure 6: PFD(t) / PFDAVG for [C4]



**Figure 7: PFD(t) / PFD AVG for [C5]**



**Figure 8: PFD(t) / PFD AVG for [C6]**



## 6 Terms and Definitions

Internal Diagnostics	Tests performed internally by the device or, if specified, externally by another device without manual intervention.
Fault tolerance	Ability of a functional unit to continue to perform a required function in the presence of faults or errors (IEC 61508-4, 3.6.3).
DC / DC <sub>avg</sub>	Diagnostic Coverage of dangerous failures (in %)
FIT	Failure In Time ( $1 \times 10^{-9}$ failures per hour)
FMEDA	Failure Modes, Effects, and Diagnostic Analysis
HFT	Hardware Fault Tolerance A hardware fault tolerance of N means that N+1 is the minimum number of faults that could cause a loss of the safety function.
High demand mode	Mode, where the safety function is only performed on demand, in order to transfer the EUC into a specified safe state, and where the frequency of demands is greater than one per year.
Low demand mode	Mode, where the safety function is only performed on demand, in order to transfer the EUC into a specified safe state, and where the frequency of demands is no greater than one per year.
MTTF <sub>D</sub>	Mean Time To dangerous Failure
PFD <sub>AVG</sub>	Average Probability of Failure on Demand
PFH	Probability of dangerous Failure per Hour
PL	Performance Level ISO 13849-1: Discrete level used to specify the ability of safety-related parts of control systems to perform a safety function under foreseeable conditions.
SFF	Safe Failure Fraction, summarizes the fraction of failures which lead to a safe state plus the fraction of failures which will be detected by automatic diagnostic measures and lead to a defined safety action.
SIF	Safety Instrumented Function
SIL	Safety Integrity Level IEC 61508: discrete level (one out of a possible four), corresponding to a range of safety integrity values, where safety integrity level 4 has the highest level of safety integrity and safety integrity level 1 has the lowest. IEC 62061: discrete level (one out of a possible three) for specifying the safety integrity requirements of the safety-related control functions to be allocated to the SRECS, where safety integrity level three has the highest level of safety integrity and safety integrity level one has the lowest.
SIS	Safety Instrumented System – Implementation of one or more Safety Instrumented Functions. A SIS is composed of any combination of sensor(s), logic solver(s), and final element(s).
Type B element	“Complex” element (using complex components such as micro controllers or programmable logic); for details see 7.4.4.1.3 of IEC 61508-2
T[Proof]	Proof Test Interval

## 7 Status of the document

### 7.1 Liability

*exida* prepares reports based on methods advocated in International standards. Failure rates are obtained from a collection of industrial databases. *exida* accepts no liability whatsoever for the use of these numbers or for the correctness of the standards on which the general calculation methods are based.

Due to future potential changes in the standards, best available information and best practices, the current FMEDA results presented in this report may not be fully consistent with results that would be presented for the identical product at some future time. As a leader in the functional safety market place, *exida* is actively involved in evolving best practices prior to official release of updated standards so that our reports effectively anticipate any known changes. In addition, most changes are anticipated to be incremental in nature and results reported within the previous three year period should be sufficient for current usage without significant question.

Most products also tend to undergo incremental changes over time. If an *exida* FMEDA has not been updated within the last three years and the exact results are critical to the SIL verification, you may wish to contact the product vendor to verify the current validity of the results.

## 7.2 Releases

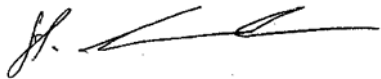
Version History: V3R4: Added Appendix 5 with typical failure rates of thermocouples for the failure modes “open circuit”, “short circuit” and “temperature drift”; September 26, 2024  
V3R3: Corrected after review by customer; April 09, 2024  
V3R2: Added Soft Errors to the FMEDA; February 16, 2024  
V3R1: Merged AU and AD failures to general annunciation failures. Those are not part of the analysis; February 1<sup>st</sup>, 2024  
V3R0: Updated to IEC 61508:2010; Route 2H, Includes metrics according to ISO 13849-1; December 22, 2023  
V2R1: Corrected Tables 21 and 32; August 11, 2015  
V2R0: Non-Ex versions added; July 8, 2014  
V1R1: Purpose and Scope section modified; September 27, 2010  
V1R0: Review comments incorporated; May 18, 2010  
V0R1: Initial version; March 31, 2010

Authors: Stephan Aschenbrenner, Piotr Serwa, Philipp Hanzik, Armin Schulze

Review: V3R4: Stephan Aschenbrenner (*exida*); September 26, 2024  
V3R0: Armin Schulze (*exida*), December 19, 2023  
V0R1: Hans Jørgen Eriksen (PR electronics A/S); April 15, 2010  
Rachel Amkreutz (*exida*); May 17, 2010

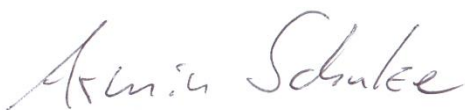
Release status: Released to PR electronics A/S

## 7.3 Release Signatures



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Dipl.-Ing. (Univ.) Stephan Aschenbrenner, Partner, CEO



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Dipl.-Ing. (Univ.) Armin Schulze, Safety Engineer

## **Appendix 1: Possibilities to reveal dangerous undetected faults during the proof test**

According to section 7.4.3.2.2 f) of IEC 61508-2, proof tests shall be undertaken to reveal dangerous faults, which are undetected by diagnostic tests.

This means that it is necessary to specify how dangerous undetected faults that have been noted during the FMEDA can be detected during proof testing.

Appendix 1 shall be considered when writing the safety manual as it contains important safety related information.

### **Appendix 1.1: Possible proof tests to detect dangerous undetected faults**

A possible proof test is described in section 10 of the safety manual ([D14]) for the 9116 Universal converter.

This test will detect approximately 95% of possible “du” failures in the transmitter and the connected sensing element.

## Appendix 2: Impact of lifetime of critical components on the failure rate

According to section 7.4.9.5 of IEC 61508-2, a useful lifetime, based on experience, should be determined and used to replace equipment before the end of useful life.

Although a constant failure rate is assumed by the *exida* FMEDA prediction method (see section 4.2) this only applies provided that the useful lifetime<sup>51</sup> of components is not exceeded. Beyond their useful lifetime, the result of the probabilistic calculation method is likely optimistic, as the probability of failure significantly increases with time. The useful lifetime is highly dependent on the subsystem itself and its operating conditions.

This assumption of a constant failure rate is based on the bathtub curve. Therefore, it is obvious that the probability calculation is only valid for components which have this constant domain and that the validity of the calculation is limited to the useful lifetime of each component.

It is assumed that early failures are detected to a huge percentage during the installation period and therefore the assumption of a constant failure rate during the useful lifetime is valid.

Table 27 shows which components with reduced useful lifetime are contributing to the dangerous undetected failure rate and therefore to the PFD<sub>AVG</sub> calculation and what their estimated useful lifetime is.

**Table 27: Useful lifetime of components with reduced useful lifetime contributing to  $\lambda_{du}$**

FMEDA	Type	Name	Useful lifetime
32 Pt100 Relay, Current Relay, Voltage Relay	Relay (w. FE) - Plastic-sealed, low gas emission, tempered plastic, single contacts (alloy on silver basis), >20cN	RE201 (Relay)	Approximately 100.000 switching cycles

Assuming one demand per year for low demand mode applications and additional switching cycles during installation and proof testing, the relays do not have a real impact on the useful lifetime.

When plant experience indicates a shorter useful lifetime than indicated in this appendix, the number based on plant experience should be used.

<sup>51</sup> Useful lifetime is a reliability engineering term that describes the operational time interval where the failure rate of a device is relatively constant. It is not a term which covers product obsolescence, warranty, or other commercial issues.

## Appendix 3: *exida* Environmental Profiles

<i>exida</i> Profile	1	2	3	4	5	6
<b>Description (Electrical)</b>	Cabinet mounted/ Climate Controlled	Low Power Field Mounted  no self-heating	General Field Mounted  self-heating	Subsea	Offshore	N/A
<b>Description (Mechanical)</b>	Cabinet mounted/ Climate Controlled	General Field Mounted	General Field Mounted	Subsea	Offshore	Process Wetted
<b>IEC 60654-1 Profile</b>	B2	C3 also applicable for D1	C3 also applicable for D1	N/A	C3 also applicable for D1	N/A
<b>Average Ambient Temperature</b>	30°C	25°C	25°C	5°C	25°C	25°C
<b>Average Internal Temperature</b>	60°C	30°C	45°C	5°C	45°C	Process Fluid Temp.
<b>Daily Temperature Excursion (pk-pk)</b>	5°C	25°C	25°C	0°C	25°C	N/A
<b>Seasonal Temperature Excursion (winter average vs. summer average)</b>	5°C	40°C	40°C	2°C	40°C	N/A
<b>Exposed to Elements/Weather Conditions</b>	No	Yes	Yes	Yes	Yes	Yes
<b>Humidity<sup>52</sup></b>	0-95% Non-Condensing	0-100% Condensing	0-100% Condensing	0-100% Condensing	0-100% Condensing	N/A
<b>Shock<sup>53</sup></b>	10 g	15 g	15 g	15 g	15 g	N/A
<b>Vibration<sup>54</sup></b>	2 g	3 g	3 g	3 g	3 g	N/A
<b>Chemical Corrosion<sup>55</sup></b>	G2	G3	G3	G3	G3	Compatible Material
<b>Surge<sup>56</sup></b>						
Line-Line	0.5 kV	0.5 kV	0.5 kV	0.5 kV	0.5 kV	N/A
Line-Ground	1 kV	1 kV	1 kV	1 kV	1 kV	
<b>EMI Susceptibility<sup>57</sup></b>						
80MHz to 1.4 GHz	10V /m	10V /m	10V /m	10V /m	10V /m	N/A
1.4 GHz to 2.0 GHz	3V/m	3V/m	3V/m	3V/m	3V/m	
2.0Ghz to 2.7 GHz	1V/m	1V/m	1V/m	1V/m	1V/m	
<b>ESD (Air)<sup>58</sup></b>	6kV	6kV	6kV	6kV	6kV	N/A

<sup>52</sup> Humidity rating per IEC 60068-2-3

<sup>53</sup> Shock rating per IEC 60068-2-27

<sup>54</sup> Vibration rating per IEC 60068-2-6

<sup>55</sup> Chemical Corrosion rating per ISA 71.04

<sup>56</sup> Surge rating per IEC 61000-4-5

<sup>57</sup> EMI Susceptibility rating per IEC 6100-4-3

<sup>58</sup> ESD (Air) rating per IEC 61000-4-2

## Appendix 4: *exida* Route 2<sub>H</sub> Criteria

IEC 61508:2010 2<sup>nd</sup> edition describes the Route 2<sub>H</sub> alternative to Route 1<sub>H</sub> architectural constraints.

The standard states:

"based on data collected in accordance with published standards (e.g., IEC 60300-3-2: or ISO 14224); and, be evaluated according to

- the amount of field feedback; and
- the exercise of **expert judgment**; and when needed
- the undertake of specific tests,

in order to estimate the average and the uncertainty level (e.g., the 90% confidence interval or the probability distribution) of each reliability parameter (e.g., failure rate) used in the calculations."

*exida* has interpreted this to mean not just a simple 90% confidence level in the uncertainty analysis, but a high confidence level in the entire data collection process. As IEC 61508:2010 2<sup>nd</sup> edition does not give detailed criteria for Route 2<sub>H</sub>, *exida* has established the following:

1. field unit operational hours of 100,000,000 per each component; and
2. a device and all of its components have been installed in the field for one year or more; and
3. operational hours are counted only when the data collection process has been audited for correctness and completeness; and
4. failure definitions, especially "random" versus "systematic" are checked by *exida*; and
5. every component used in an FMEDA meets the above criteria.

This set of requirements is chosen to assure high integrity failure data suitable for safety integrity verification.

## Appendix 5: Using the FMEDA results

The 9116 Universal converter together with a temperature sensing device becomes a temperature sensor assembly. Therefore, when using the results of this FMEDA in a SIL verification assessment, the failure rates and failure modes of the temperature sensing device must be considered.

### Appendix 5.1: 9116 Universal converter with thermocouple

The failure mode distributions for thermocouples (TC) vary in published literature but there is strong agreement that open circuit or “burn-out” failure is the dominant failure mode. While some estimates put this failure mode at 99%+, a more conservative failure rate distribution suitable for SIS applications is shown in Table 28 and Table 29 when thermocouples are supplied with the 9116 Universal converter. The drift failure mode is primarily due to T/C aging.

The 9116 Universal converter will detect a thermocouple burn-out failure and drive its output to the specified failure state.

**Table 28: Typical failure rates for thermocouples (with extension wire)**

Failure Mode Distribution	Low Stress	High Stress
Open Circuit (Burn-out)	180 FIT	720 FIT
Short Circuit (Temperature measurement in error)	10 FIT	40 FIT
Drift (Temperature Measurement in error)	10 FIT	40 FIT

**Table 29: Typical failure rates for thermocouples (close coupled)**

Failure Mode Distribution	Low Stress	High Stress
Open Circuit (Burn-out)	95 FIT	380 FIT
Short Circuit (Temperature measurement in error)	4 FIT	16 FIT
Drift (Temperature Measurement in error)	1 FIT	4 FIT

**Table 30: Thermocouple fault classification**

Failure mode	Classification
Open circuit	Dangerous detected
Short circuit	Dangerous undetected
Drift	Dangerous undetected



A complete temperature sensor assembly consisting of the 9116 Universal converter and a temperature sensing device can be modeled by considering a series subsystem where a failure occurs if there is a failure in either component. For such a system, failure rates are added.

The failure rates for the 9116 Universal converter with the thermocouple are sums of corresponding failure rates of the converter and of the thermocouple.

**Table 31: Thermocouple (with extension wire)**

Low stress environment	High stress environment
$\lambda_{dd} = 180 \text{ FIT}$	$\lambda_{dd} = 720 \text{ FIT}$
$\lambda_{du} = 10 \text{ FIT} + 10 \text{ FIT} = 20 \text{ FIT}$	$\lambda_{du} = 40 \text{ FIT} + 40 \text{ FIT} = 80 \text{ FIT}$

**Table 32: Thermocouple (close coupled)**

Low stress environment	High stress environment
$\lambda_{dd} = 95 \text{ FIT}$	$\lambda_{dd} = 380 \text{ FIT}$
$\lambda_{du} = 4 \text{ FIT} + 1 \text{ FIT} = 5 \text{ FIT}$	$\lambda_{du} = 16 \text{ FIT} + 4 \text{ FIT} = 20 \text{ FIT}$

## Appendix 5.2: 9116 Universal converter with RTD

The failure mode distribution for an RTD depends on the application with the key variables being stress level, presence (or not) of extension wire and wire configuration (2-wire/3-wire or 4-wire). The key stress variables are high vibration and frequent temperature cycling as these are known to cause cracks in the substrate leading to broken lead connection welds. Failure rate distributions are shown in Table 33 to Table 36.

The 9116 Universal converter will detect open circuit, short circuit and a certain percentage of drift RTD failures and drive their output to the specified failure state.

**Table 33 Typical failure rates for 4-Wire RTDs (with extension wire)**

<b>RTD Failure Mode Distribution</b>	<b>Low Stress</b>	<b>High Stress</b>
Open Circuit (Burn-out)	164 FIT	656 FIT
Short Circuit (Temperature measurement in error)	8 FIT	32 FIT
Drift (Temperature Measurement in error)	28 FIT <sup>59</sup>	112 FIT <sup>60</sup>

**Table 34 Typical failure rates for 4-Wire RTDs (close coupled)**

<b>RTD Failure Mode Distribution</b>	<b>Low Stress</b>	<b>High Stress</b>
Open Circuit (Burn-out)	41.5 FIT	166 FIT
Short Circuit (Temperature measurement in error)	2.5 FIT	10 FIT
Drift (Temperature Measurement in error)	6 FIT <sup>61</sup>	24 FIT <sup>62</sup>

**Table 35 Typical failure rates for 2/3-Wire RTDs (with extension wire)**

<b>RTD Failure Mode Distribution</b>	<b>Low Stress</b>	<b>High Stress</b>
Open Circuit (Burn-out)	75 FIT	299.5 FIT
Short Circuit (Temperature measurement in error)	2 FIT	7.7 FIT
Drift (Temperature Measurement in error)	19 FIT	76.8 FIT

**Table 36 Typical failure rates for 2/3-Wire RTDs (close coupled)**

<b>RTD Failure Mode Distribution</b>	<b>Low Stress</b>	<b>High Stress</b>
Open Circuit (Burn-out)	38 FIT	151.7 FIT
Short Circuit (Temperature measurement in error)	1.4 FIT	5.7 FIT
Drift (Temperature Measurement in error)	8.6 FIT	34.6 FIT

**Table 37: RTD fault classification**

<b>Failure mode</b>	<b>Classification</b>
Open circuit	Dangerous detected
Short circuit	Dangerous detected
Drift (2/3-Wire)	Dangerous undetected
Drift (4-Wire)	Most of it is dangerous detected, remaining part dangerous undetected (assuming a correct use of 4-wire RTD)

<sup>59</sup> It is assumed that 26 FIT are detectable if the 4-wire RTD is correctly used.

<sup>60</sup> It is assumed that 104 FIT are detectable if the 4-wire RTD is correctly used.

<sup>61</sup> It is assumed that 3.5 FIT are detectable if the 4-wire RTD is correctly used.

<sup>62</sup> It is assumed that 14 FIT are detectable if the 4-wire RTD is correctly used.

A complete temperature sensor assembly consisting of 9116 Universal converter and a temperature sensing device can be modeled by considering a series subsystem where a failure occurs if there is a failure in either component. For such a system, failure rates are added.

**4-wire RTD with extension wire:**

Low stress environment	High stress environment
$\lambda_{dd} = 164 \text{ FIT} + 8 \text{ FIT} + 26 \text{ FIT} = 198 \text{ FIT}$	$\lambda_{dd} = 656 \text{ FIT} + 32 \text{ FIT} + 104 \text{ FIT} = 792 \text{ FIT}$
$\lambda_{du} = 2 \text{ FIT}$	$\lambda_{du} = 8 \text{ FIT}$

**4-wire RTD close coupled:**

Low stress environment	High stress environment
$\lambda_{dd} = 41.5 \text{ FIT} + 2.5 \text{ FIT} + 3.5 \text{ FIT} = 47.5 \text{ FIT}$	$\lambda_{dd} = 166 \text{ FIT} + 10 \text{ FIT} + 14 \text{ FIT} = 190 \text{ FIT}$
$\lambda_{du} = 2.5 \text{ FIT}$	$\lambda_{du} = 10 \text{ FIT}$

**2/3-wire RTD with extension wire:**

Low stress environment	High stress environment
$\lambda_{dd} = 75 \text{ FIT} + 2 \text{ FIT} = 77 \text{ FIT}$	$\lambda_{dd} = 299.5 \text{ FIT} + 7.7 \text{ FIT} = 307.2 \text{ FIT}$
$\lambda_{du} = 19 \text{ FIT}$	$\lambda_{du} = 76.8 \text{ FIT}$

**2/3-wire RTD close coupled:**

Low stress environment	High stress environment
$\lambda_{dd} = 38 \text{ FIT} + 1.4 \text{ FIT} = 39.4 \text{ FIT}$	$\lambda_{dd} = 151.7 \text{ FIT} + 5.7 \text{ FIT} = 157.4 \text{ FIT}$
$\lambda_{du} = 8.6 \text{ FIT}$	$\lambda_{du} = 34.6 \text{ FIT}$